

6. FÜÜSIKALISTE SÜSTEEMIDE MODELLEERIMINE

Põhiidee: on olemas reeglid, mis fikseerivad
põhimõtted jättes piisava vabaduse

3 astet:

1. Klassikaline dünaamika 1687

Newton, Hamilton, ...

isoleeritud osakesed, mehaanika reeglid
kriitika – ainult vastasmõju, interaktsioon?
siiski keerulised tulemused (3 keha probleem)

2. Termodünaamika – 1850 2. seadus

isoleeritud süsteemi entroopia saab ainult kasvada
kuni süsteem jõuab termodünaamilise tasakaaluni

lisandus pöördumatus (irreversibility)

kõik pöördumatud protsessid lisavad entroopiat

3. Dissipatiivsete struktuuride (hajasstruktuuride) teooria

koherentsed arenevad struktuurid

avatud süsteem ammutab energiat ümbritsevast süsteemist ja
ekspordib entroopiat

I. Prigogine

Erinevus 3 tasandi vahel

1. klassikaline dünaamika

aja sümmeetria rikkumine

kausaalsuse printsiip

2. termodünaamika

aja ja ruumi
sümmeetria rikkumine

printsiip: fluktuatsioonid
tekivad

3. dissipatiivsete struktuuride teooria

vt.

E. Jantsch The Self-Organizing Universe

Pergamon, Oxford et al 1980

I. Prigogine, J. Stengers. "Order out of Chaos",

Heinemann, London, 1984.

6.1 PIDEV KESKKOND

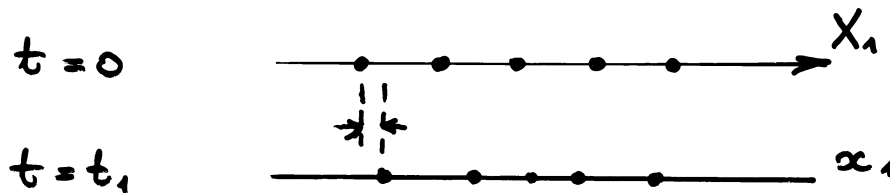
Põhi- printsübid	Alg- oletused	Aeg ja ruum
	Jäävus- seadused	Põhi- aksioomid
Teooria	Lisa – postulaadid	Alg- tingimused, oleku- võrrandite struktuur
		Suletud süsteem
Mudel	Lisa- oletused	Muutujate iseloom
		Oleku- võrrandite lõplik kuju
		Oleku- võrrandite või vaba energia funktsiooni aproksi- meerimine
		Mate- maatiline mudel

6.1. PIDEV KESKKOND

ALGOLETUSED

- (i) aeg – absoluutne aeg t ;
- (ii) ruum – kolmemõõtmeline (3D) Eukleidese ruum;
- (iii) materia makroskoopiline hulk – liikuvate osakeste pidev hulk, mis meelevaldsel ajahetkel $t = const$ on ruumi osas B, millel on pind A ja maht $V \neq 0$ ning positiivne mass M .

Liikumine



$$3D: x_k = x_k(X_1, X_2, X_3; t)$$

$$X_k = X_k(x_1, x_2, x_3; t)$$

$$k = 1, 2, 3$$

üheselt määratud teisendused

Tähistus:
$$x_{i,k} = \frac{\partial x_i}{\partial X_k}$$

JÄÄVUSSEADUSED (lihtsustatud)

1. Massi jäävuse seadus

$$\int_V \rho_0 dV = \int_v \rho dv \quad \text{integraalkuju}$$

ρ_0, ρ tihedus
 V, v maht

$$\frac{\partial \rho}{\partial t} + (\rho v_i)_{,i} = 0 \quad \text{diferentsiaalikuju}$$

v_i – kiiruse komponendid

2. Impulsi jäävuse seadus (Newtoni II seadus)

$$T_{ij,i} + \rho_0(f_j - A_j) = 0$$

T_{ij} – pingetensor
 f_j – mahujõud
 A_j – kiirendusvektori
komponendid

3. Kineetilise momendi jäävus

$$T_{ij} = T_{ji} \quad \text{ehk nihkepingete paarilisus}$$

4. Energia jäävus

$$\rho \frac{d\varepsilon}{dt} = T_{ij} \dot{E}_{ij} + Q_{K,K} + \rho_0 h$$

E_{ij} – deformatsioonitensor

\dot{E}_{ij} – deformatsiooni kiirus

Q_k – soojushulk

h – lisa soojusallikas

Lisa: entroopia võrratus

$$T_{ij} \dot{E}_{ij} + \frac{1}{T} Q_k T_{,k} - \rho_0 \dot{F} - \rho_0 \dot{T} S \geq 0$$

T – temperatuur

S – entroopia

F – nn Helmholtzi vaba energia

LISAPOSTULAADID

1) Postulaat algolukorrast ajal $t = 0$:

$$\dot{U}_k = 0, \quad T_{kl} = 0, \quad Q_k = 0$$

(U_k – siire \rightarrow ($x_k - X_k$))

vaba energia $F = F_0, \quad F_0 = \text{const.}$

temperatuur $T = T_0, \quad T_0 = \text{const.}$

vaba energia $F = E - TS$

2) postulaat olekuvõrranditest
(mis millest sõltub)

(i) $F = F(K_1, K_2, K_3; T)$

K_i – deformatsioonitensori invariandid

T – temperatuur

(ii) pingetensor = pöörduv osa + pöördumatu osa
(elastne) (dissipatiivne)

$$T_{kl}^e = \rho_0 \frac{\partial F}{\partial E_{kl}} \quad - \text{pöörduv osa}$$

$$T_{kl}^d = T_{kl}^d(\dot{E}_{kl}) \quad - \text{pöördumatu osa}$$

(iii) soojusjuhtivus (Fourier' seadus)

SULETUD SÜSTEEM

$$\mathbf{T}_{ij,i} + \rho_0 (\mathbf{f}_i - \ddot{\mathbf{U}}_j) = 0 \quad \text{liikumine}$$

$$\rho_0 \mathbf{T} \left(\frac{\partial^2 \mathbf{F}}{\partial \mathbf{T} \partial \mathbf{E}_{kl}} \dot{\mathbf{E}}_{kl} + \frac{\partial^2 \mathbf{F}}{\partial \mathbf{T}^2} \dot{\mathbf{T}} \right) + \mathbf{T}_{kl}^d \dot{\mathbf{E}}_{kl} + \\ + \mathbf{Q}_{k,k} + \rho_0 \mathbf{h} = 0 \quad \text{energia}$$

$$\mathbf{Q}_i = \mathbf{k}_{ij} \mathbf{T}_{,j} \quad \text{Fourier' seadus}$$

$$\mathbf{T}_{kl} = \mathbf{T}_{kl}^e + \mathbf{T}_{kl}^d \quad \text{lisapostulaat}$$

$$\mathbf{F} = \mathbf{F}(\mathbf{K}_1, \mathbf{K}_2, \mathbf{K}_3; \mathbf{T}) \quad \text{lisapostulaat}$$

$$\mathbf{T}_{kl}^e = \rho_0 \frac{\partial \mathbf{F}}{\partial \mathbf{E}_{kl}} \quad \text{lisapostulaat}$$

$$\mathbf{T}_{kl}^d = \mathbf{a}_{0l} \cdot \dot{\mathbf{E}}_{kl} \quad \text{lisapostulaat} \\ \text{(aproksimatsioon)}$$

$$\mathbf{E}_{ij} = \frac{1}{2} (\mathbf{U}_{i,j} + \mathbf{U}_{j,i} + \mathbf{U}_{m,j} \cdot \mathbf{U}_{m,i})$$

deformatsioonitensor väljendatud siirde (paigutise)

tuletiste kaudu

LISAOLETUSED

$$\begin{aligned}
 U_{i,j} \ll 1 & \quad \text{väikesed deformatsioonid} \\
 |T - T_0| T_0^{-1} \ll 1 & \quad \text{väike temperatuurimuutus} \\
 & \quad \text{(NB! ohtlik oletus!)}
 \end{aligned}$$

$$\begin{aligned}
 F(\mathbf{E}_{kl}, T) = & F(0, T_0) + \\
 & + \frac{\partial F(0, T_0)}{\partial \mathbf{E}_{kl}} \mathbf{E}_{kl} + \frac{\partial F(0, T_0)}{\partial T} T + \\
 & + \frac{1}{2} \frac{\partial^2 F(0, T_0)}{\partial \mathbf{E}_{kl} \partial \mathbf{E}_{ij}} \mathbf{E}_{kl} \mathbf{E}_{ij} + \\
 & + \frac{1}{2} \frac{\partial^2 F(0, T_0)}{\partial \mathbf{E}_{kl} \partial T} \mathbf{E}_{kl} (T - T_0) + \\
 & + \frac{1}{2} \frac{\partial^2 F(0, T_0)}{\partial T^2} (T - T_0)^2 + \\
 & \dots
 \end{aligned}$$

Harilik rittaarendus tasakaaluoleku $(0, T_0)$
suhtes, nn. MacLaureni rida

Tuletised on konstandid!

$$\begin{aligned}
 \rho_0 F = & \frac{1}{2} \lambda \mathbf{K}_1^2 + \mu \mathbf{K}_2 + \quad (\text{kõrgemat järku liikmed}) + \\
 & + \kappa \mathbf{K}_1 (T - T_0) + \kappa_1 (T - T_0)^2
 \end{aligned}$$

$$\left. \begin{aligned}
 \mathbf{K}_1 &= \mathbf{E}_{ii} \\
 \mathbf{K}_2 &= \mathbf{E}_{ij} \mathbf{E}_{ij}
 \end{aligned} \right\} \begin{array}{l} \lambda, \mu \\ \kappa, \kappa_1 \end{array} \text{ konstandid}$$

MATEMAATILINE MUDEL

$$\rho_0 \ddot{U}_n - C_{nkml} U_{k,lm} - D_{nkml} \dot{U}_{k,lm} = B_{nk} T_{,k}$$

$$g\dot{T} + H_{mn} \dot{U}_{m,n} = Q_{k,k}$$

$$Q_n = kT_{,n}$$

$$\rho_0, \quad C_{nkml}, \quad D_{nkml}, \quad B_{nk}, \quad g, \quad H_{mn}, \quad k$$

konstandid lihtsaimal juhul

kuid võivad olla funktsioonid

$$(X_i, t, U_i, T)$$

OLULINE:

Jäävusseadused + olekuvõrrandid
määratakse eksperimentidist

ELEKTRODÜNAAMIKA

E – elektriväli

J – vool

P – polarisatsioon

H – magnetväli

M – magneetumine

\vec{V} – kiirus

q_e – laeng

$$D = E + P$$

$$B = H + M$$

$$M = M + \frac{1}{c} v \times P$$

$$H = H - \frac{1}{c} v \times D$$

$$B = B - \frac{1}{c} v \times E$$

$$\mathfrak{J} = J - q_e v$$

$$E = E + \frac{1}{c} v \times B$$

Maxwelli võrrandid

$$\nabla \cdot D - q_e = 0$$

$$\nabla \times E + \frac{1}{c} \frac{\partial B}{\partial t} = 0$$

$$\nabla \cdot B = 0$$

$$\nabla \times H - \frac{1}{c} \frac{\partial D}{\partial t} = \frac{1}{c} J$$

$$\frac{\partial q_e}{\partial t} + \nabla \cdot J = 0$$

Termomehaanikalised jäävusseadused

mass $\dot{\rho} + \rho \nabla \cdot \mathbf{v} = 0$

impulss $t_{kl,k} + \rho (f_l - \dot{v}_l) + F_l^E = 0$

moment $t_{[kl]} = E_{[k} P_{l]} + B_{[k} M_{l]}$

energia $\rho (\dot{\psi} + \dot{\theta} \eta + \theta \dot{\eta}) - t_{kl} v_{k,l} - \nabla \cdot \mathbf{q} - \rho h +$
 $+ P_k \dot{E}_k + M_k \dot{B}_k - \mathfrak{S}_k E_k = 0$

entroopia $\rho \gamma \equiv \rho \dot{\eta} - \nabla \cdot (\mathbf{q} / \theta) - (\rho h / \theta) \geq 0$

6.2 MEHAANIKA

JÄIGA KEHA MEHAANIKA

Jäävusseadused:

1. Energia on jääv

$$E = U + K$$

potentsiaalne kineetiline
energia

2. Impulss \mathbf{P} on jääv

3. Masskeskpunkti kiirus \mathbf{V} on jääv

koordinaat

$$R = \sum_i m_i r_i / \sum_i m_i$$

$$P = \sum_i m_i v_i = M \frac{dR}{dt} = M V$$

4. Kineetiline moment \mathbf{L} on jääv

10 jäävusseadust

energia	1	
impulss	3	komponenti
kiirus	3	komponenti
kineetiline moment	3	komponenti

Jäiga ja deformeeruva keha võrdlus

	JÄIK	DEFORMEERUV
Massi jäävus	Tagatud definiitsiooni kohaselt	$\frac{\partial \rho}{\partial t} + (\rho v_i)_{,i} = 0$
Liikumishulga jäävus	$\frac{d\vec{k}}{dt} = \vec{F}$	$T_{ij,i} - \rho a_i = 0$
Kineetilise momendi jäävus	$\frac{d\vec{h}_o}{dt} = \vec{M}$	$T_{ij} = T_{ji}$
Energia	$\frac{dK}{dt} = \frac{dW^e}{dt} + \frac{dW^i}{dt}$	$\rho \frac{d\varepsilon}{dt} = \frac{1}{2} (v_{r,p} + v_{p,r}) T_{pr} + Q_{p,p}$
Olekuvõrrand	Keha on jäik	$T_{ij} = T_{ij}(u_{m,n})$

Descartes'i koordinadid

W^e välisjõudude töö

W^i sisejõudude töö

K kineetiline energia

6.3 ÜLDISED IDEED

Hamiltoni funktsioon

$$E = T + U = H$$

kineetiline energia potentsiaalne energia Lagrange'i funktsioon

$$L = \sum_i p_i \dot{q}_i - U$$

q_i – üldistatud muutuja
 p_i – sellele vastav impulss

liikumisvõrrandid

$$\begin{cases} \frac{dp_i}{dt} + \frac{\partial H}{\partial q_i} = 0 \\ \frac{dq_i}{dt} - \frac{\partial H}{\partial p_i} = 0 \end{cases}$$

Sisemuutujad

Vaadeldavad (observable) ehk mõõdetavad muutujad

siire
deformatsioon
pinge / surve
temperatuur
....

Sisemuutujad (internal variables)

termodünaamilised parameetrid
fenomenoloogilised parameetrid
e. muutujad

	Mõõdetavad muutujad	Sisemuutuja(d)
nemaatilised kristallid	surve	suunavektor
plastsusteooria	deformatsioon	purunemisparameeter
närviimpulss	potentsiaal (s.o. pinge)	ioonvoolu parameetrid

Klassikaline:

Mõõdetavad muutujad	Sise-muutuja(d)
kehtivad jäävusseadused, alluvad inertsile liikumisvõrrandid vaja teada Helmholtzi vaba energiat F u	ei allu inertsile difusioonvõrrandid kineetilised võrrandid vaja teada dissipatsioonipotentsiaali w
$\frac{\partial^2 \mathbf{u}}{\partial t^2} - \frac{\partial^2 \mathbf{u}}{\partial \mathbf{x}^2} = \mathbf{f}(\mathbf{u}, \mathbf{w})$	$\frac{\partial \mathbf{w}}{\partial t} = \frac{\partial^2 \mathbf{w}}{\partial \mathbf{x}^2} + \mathbf{g}(\mathbf{w}, \mathbf{u})$

Sisemuutujate inerts? Vt. näide

Modifitseeritud:

Mõõdetavad muutujad	Sise-muutuja(d)
	alluvad inertsile
	$\frac{\partial^2 \mathbf{w}}{\partial t^2} = \frac{\partial^2 \mathbf{w}}{\partial \mathbf{x}^2} + \mathbf{g}(\mathbf{w}, \mathbf{u})$

Vt. mikrostruktuuriga materjalid (Berezovski, Engelbrecht)

Põhinõuded olekuvõrranditele

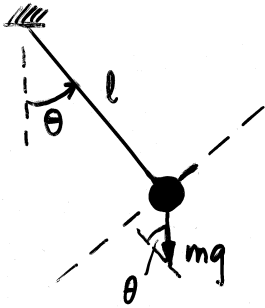
Põhjuslikkus	Causality	
Määratus	Determinism	
Võrdesitatus	Equipresence	kõik muutujad võrdsõltuvad
Objektiivsus	Objectivity	taustsüsteem ei tohi muuta
Aja pööratavus	Time reversal	$t \rightarrow -t$?
Keskkonna invariantsus	Material invariance	
Lokaalsuse printsiip	Neighbourhood	kauge ruum ei mõju ?
Mälu printsiip	Memory	kauge aeg ei mõju ?
Sobivus	Admissibility	olekuvõrrandid ei ole vastuolus jäävusseaduste ja entroopia tingimustega

ÜLDINE JÄÄVUSSEADUS

$$\begin{aligned} \text{Muutuja kogus} &= \text{muutuja kogus} \\ \text{antud ajahetkel} &= \text{eelmisel ajahetkel} \\ &+ \text{kogus, mis on loodud} \\ &+ \text{ajaintervalli jooksul} \\ &- \text{kogus, mis on hävitatud} \\ &- \text{ajaintervalli jooksul} \\ &+ \text{juurdevool süsteemi} \end{aligned}$$

$$\begin{aligned} \text{antud} &= \text{eelmine} \\ \text{ajahetk} &- \text{ajahetk} &= \text{aja intervall} \end{aligned}$$

Näide: Pendel



Liikumisvõrrand

$$ml\ddot{\theta} + mg \sin\theta = 0$$

$$\ddot{\theta} + k^2 \sin\theta = 0$$

$$k^2 = \frac{g}{l}$$

$$\sin\theta = \theta - \frac{\theta^3}{3!} + \frac{\theta^5}{5!} + \dots$$

$$\ddot{\theta} + k^2 \left(\theta - \frac{\theta^3}{3!} + \frac{\theta^5}{5!} + \dots \right) = 0$$

$$\ddot{\theta} + k^2\theta = 0$$

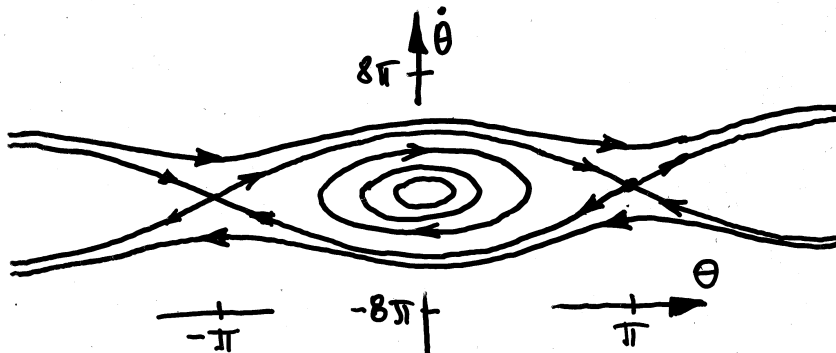
$$T \cong 2\pi \sqrt{\frac{l}{g}} \left(1 + \frac{1}{16} \theta_0^2 + \frac{11}{3072} \theta_0^4 + \dots \right)$$

$$\varphi^0 \quad \frac{1}{16} \theta_0^2 \quad \frac{11}{3072} \theta_0^4$$

$$10^\circ \quad 0.002 \quad 3 \cdot 10^{-6}$$

$$20^\circ \quad 0.0076 \quad 1 \cdot 10^{-4}$$

$$30^\circ \quad 0.039 \quad 1.4 \cdot 10^{-3}$$



Transpordivoogude modelleerimine



$$\text{kiirus} = \frac{\text{tee pikkus}}{\text{aeg}} \quad v = \frac{dx}{dt}$$

$$\text{voog : } q = \frac{\text{arv}}{\text{tunnis}} \quad \text{tihedus : } \rho = \frac{\text{arv}}{\text{km kohta}}$$

$$\text{voog} = \text{tihedus} \times \text{kiirus} \quad q = \rho \cdot v$$

$$\text{voo jäävus intervallis} \quad \begin{array}{c} | \text{---} | \\ \text{a} \qquad \text{b} \end{array} \quad x$$

$$\text{arv intervallis:} \quad N = \int_a^b \rho(x, t) dx$$

$$\text{muutus:} \quad \frac{dN}{dt} = q(a, t) - q(b, t)$$

$$\text{jäävus:} \quad \frac{d}{dt} \int \rho(x, t) dx = q(a, t) - q(b, t)$$

$$\text{siit} \quad \frac{\partial \rho}{\partial t} + \frac{\partial q}{\partial x} = 0 \quad \text{ehk} \quad \frac{\partial \rho}{\partial t} + \frac{\partial}{\partial x} (\rho v) = 0$$

Pidev keskkond,

$$\text{massi jäävus} \quad \frac{\partial \rho}{\partial t} + \frac{\partial}{\partial x} (\rho v) = 0$$

Balance laws

Canonical (material) momentum balance

$$\left. \frac{\partial \mathbf{P}}{\partial t} \right|_{\mathbf{x}} - \text{Div}_R \mathbf{b} = \mathbf{f}^{int} + \mathbf{f}^{ext} + \mathbf{f}^{inh}$$

\mathbf{P} – material momentum, \mathbf{b} – material Eshelby stress,
material inhomogeneity force – \mathbf{f}^{inh} ,
material external (body) force – \mathbf{f}^{ext} ,
material internal force – \mathbf{f}^{int} .

Energy conservation

$$\frac{\partial(S\theta)}{\partial t} \Big|_{\mathbf{x}} - \nabla_R \cdot \mathbf{Q} = h^{int}, \quad h^{int} := \mathbf{T} : \dot{\mathbf{F}} - \frac{\partial W}{\partial t} \Big|_{\mathbf{x}}$$

the second law

$$\mathbf{S}\dot{\theta} + \mathbf{S} \cdot \nabla_R \theta \leq h^{int} + (\theta \mathbf{K}) \quad S\dot{\theta} + \mathbf{S} \cdot \nabla_R \leq h^{int} + (\theta \mathbf{K})$$

\mathbf{S} – the entropy flux, S – the entropy density per unit reference volume,
 θ – absolute temperature, \mathbf{K} – extra entropy flux,
 \mathbf{T} – the first Piola – Kirchhoff tensor, \mathbf{F} – deformation gradient.

Internal variables (1)

Observable – strains, displacements, etc.

internal – describe the internal structure of the material

see Maugin, Muschik, 1994

- damage parameter
- orientation of liquid crystals
- dislocations
- etc.

In this formalism : internal variables might not be inertial

Internal variables (2)

Microstructured solids

Single / dual variables

Berezovski, Engelbrecht, Maugin, 2008

Dual variables α , β — second order tensors

Free energy W

$$W = \bar{W}(\mathbf{F}, \theta, \boldsymbol{\alpha}, \nabla_{\mathbf{R}} \boldsymbol{\alpha}, \boldsymbol{\beta}, \nabla_{\mathbf{R}} \boldsymbol{\beta})$$

Internal variables (3)

From dissipation inequality

$$\begin{pmatrix} \dot{\alpha} \\ \dot{\beta} \end{pmatrix} = \mathbf{L} \begin{pmatrix} \tilde{A} \\ \tilde{B} \end{pmatrix} = \begin{pmatrix} \mathbf{L}^{11} & \mathbf{L}^{12} \\ \mathbf{L}^{21} & \mathbf{L}^{22} \end{pmatrix} \begin{pmatrix} \tilde{A} \\ \tilde{B} \end{pmatrix}$$

\mathbf{L} – depend on state variables

\tilde{A}, \tilde{B} related to \bar{W}

A simple non-dissipative process

$$\dot{\alpha} = \mathbf{L}^{12} \tilde{B}, \quad \dot{\beta} = -\mathbf{L}^{12} \tilde{A}$$

A special case \bar{W} independent of $\nabla_{\mathbf{R}} \beta$

$$\ddot{\alpha} = (\mathbf{L}^{12} \cdot \mathbf{L}^{12}) \tilde{A}$$

inertia account

Mindlin model

Mindlin model

two balance laws

$$\begin{aligned}\rho_0 u_{tt} &= a u_{xx} + A \psi_x \\ I \psi_{tt} &= C \psi_{xx} - A u_x - B \psi\end{aligned}$$

Ψ – microdeformation

Internal variable

one balance law

dissipation inequality

Ψ – internal variable

Hierarchy waves

System of two 2nd order equations \rightarrow one 4th order equation

$$u_{tt} = (c_0^2 - c_A^2)u_{xx} - p^2 \underbrace{(u_{tt} - c_0^2 u_{xx})}_{tt} + p^2 c_1^2 \underbrace{(u_{tt} - c_0^2 u_{xx})}_{xx}$$

Simplified (slaving principle)

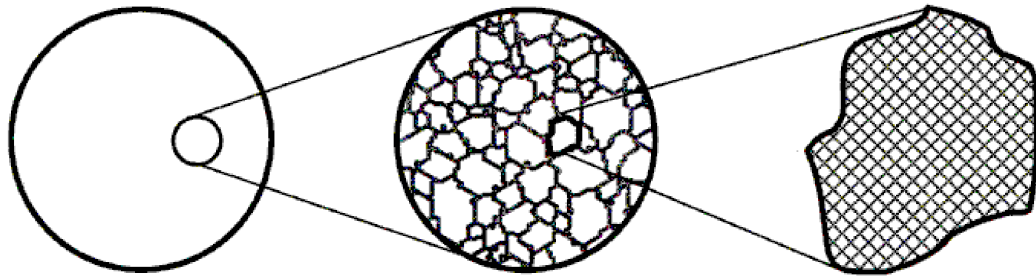
$$u_{tt} = (c_0^2 - c_A^2)u_{xx} - p^2 c_A^2 \underbrace{(u_{tt} - c_1^2 u_{xx})}_{xx}$$

Multiple scales

macrostructure

microstructure 1

microstructure 2



Multiple scales

$$\begin{aligned}
 u_{tt} = & (c_0^2 - c_A^2) u_{xx} + p_1^2 c_{A1}^2 \underbrace{\left[u_{tt} - (c_1^2 - c_{A2}^2) u_{xx} \right]}_{xx} - \\
 & - p_1^2 c_{A1}^2 \underbrace{p_2^2 c_{A2}^2 (u_{tt} - c_2^2 u_{xx})}_{xxxx}
 \end{aligned}$$

Nonlinearities

free energy W – cubic

model

$$\rho u_{tt} = \alpha u_{xx} + N u_x u_{xx} + A \psi_x$$

$$I \psi_{tt} = C \psi_{xx} + M \psi_x \psi_{xx} - A u_x - B \psi$$

hyperbolic wave equation \rightarrow two waves
evolution equation \rightarrow one-wave equations

Separation techniques:

Taniuti, Nishihara 1977, 1983

Jeffrey, Kawahara 1982

Engelbrecht 1983

Evolution equation

KdV $u_\tau + kuu_\xi + du_{\xi\xi\xi} = 0$

mKdV $u_\tau + [P(u)]_\xi + du_{3\xi} + bu_{5\xi} = 0$

$$P(u) = -\frac{1}{2}u^2 + \frac{1}{4}u^4$$

microstructured solids $u_\tau + qvv_\xi + dv_{\xi\xi\xi} + r\left(v_\xi^2\right)_{\xi\xi} = 0$

Näide : LUMI JA SUUSATAMINE

Lume struktuur

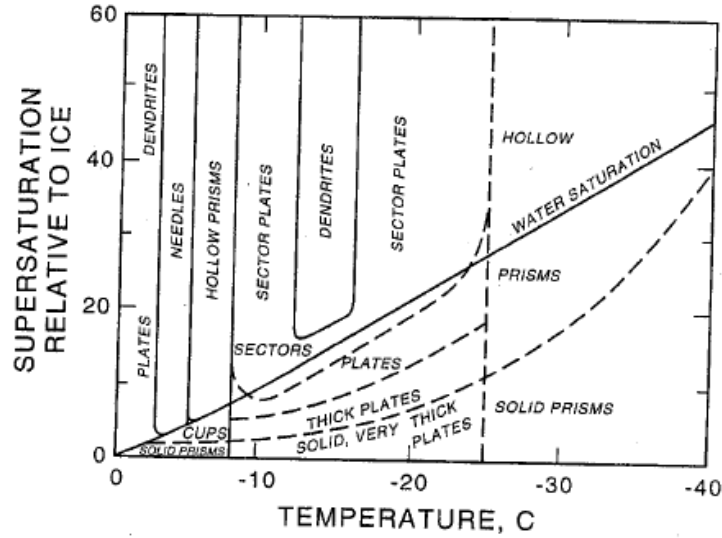


FIGURE 2.3. Atmospheric snow crystal types given as functions of the temperature and supersaturation relative to a flat ice surface at the moment of their formation. (From J. B. Mason, 1971, *The Physics of Clouds*, 2nd ed., Oxford, UK: Clarendon Press. By permission of Oxford University Press.)

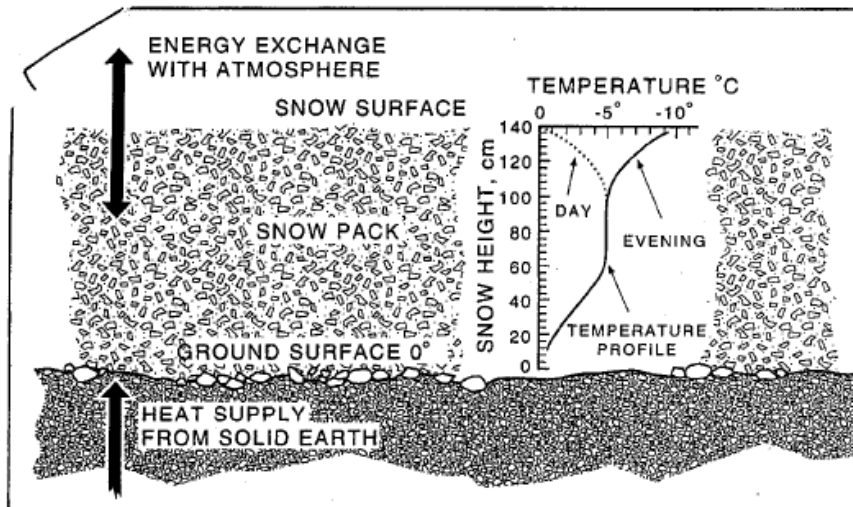


FIGURE 2.8. Temperature profile of a snowpack. Temperature gradients exist at the top and at the bottom, near the surface of the snowpack and at the ground surface. In the middle, the snowpack is at an equitemperature state (Perla and Martinelli, 1979).

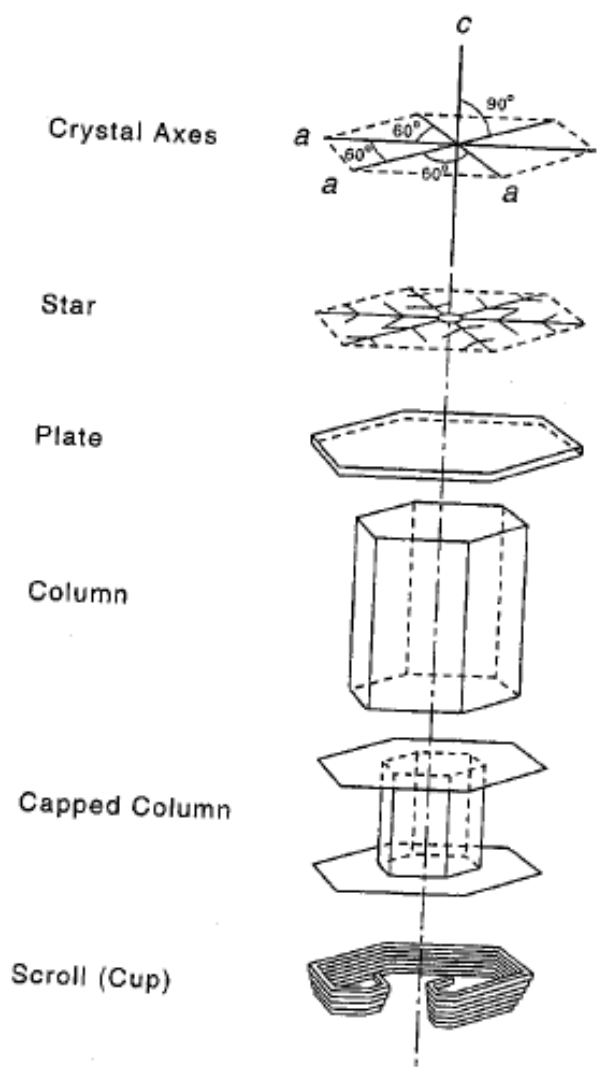
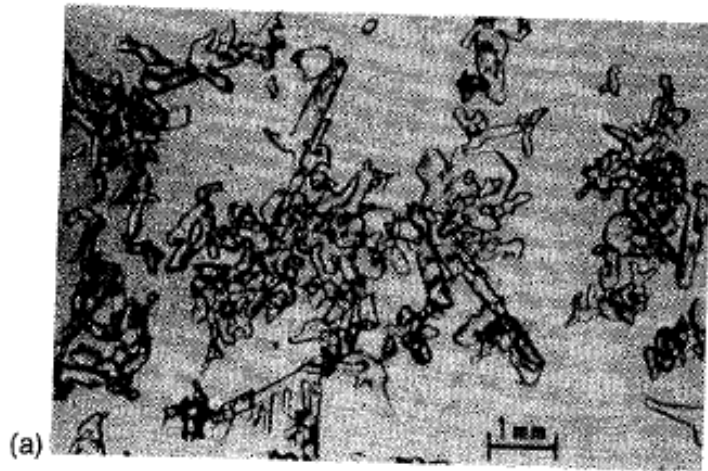


FIGURE 2.2. Principal types of atmospheric snow crystals shown in relation to the crystal axes of ice (Perla and Martinelli, 1979).



(a)

FIGURE 2.6. Equitemperature (ET) metamorphism of newly fallen snow. The faceted, dendritic arms of the new snow grains in the left frame have disappeared in the right frame, metamorphosing into rounded, sintered grains. (Reprinted with permission from Colbeck *et al.*, 1990. Photographs courtesy of E. Akitaya.)



(b)

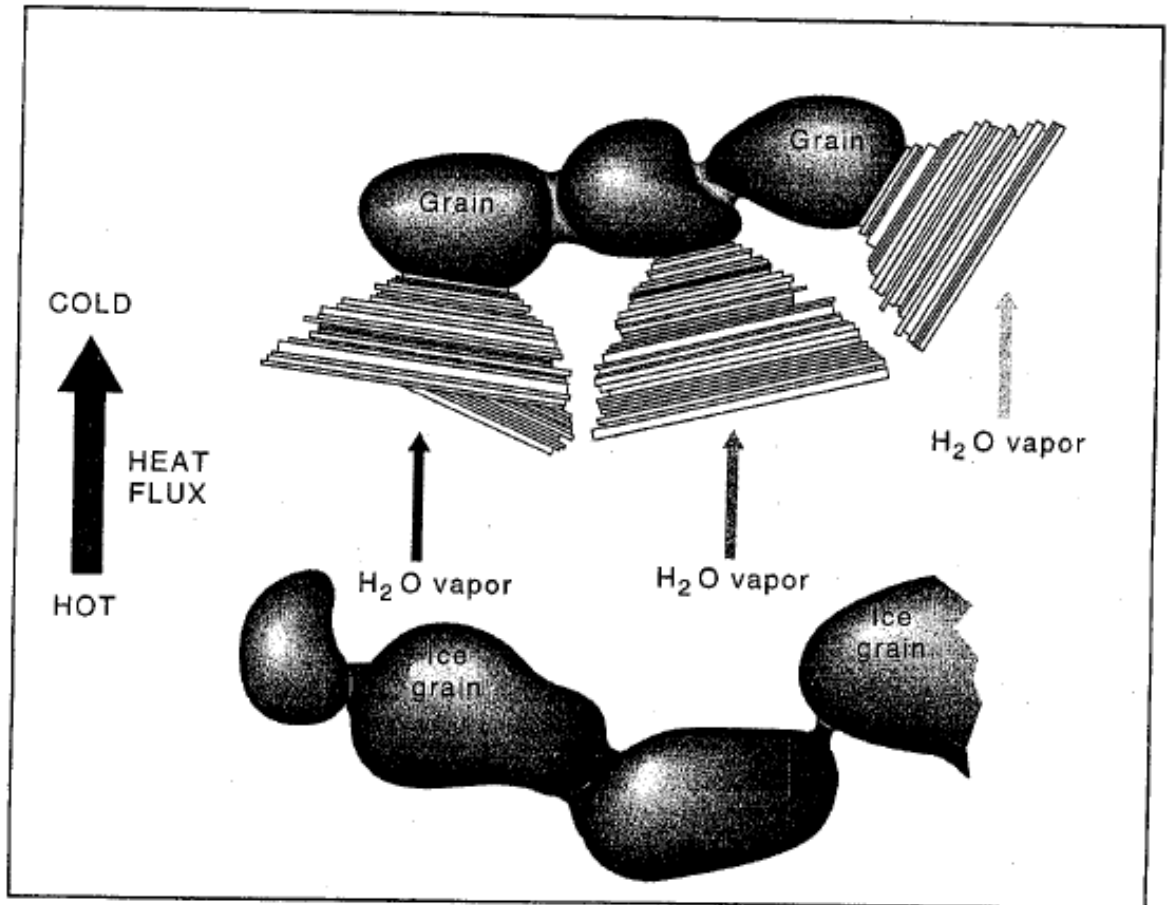


FIGURE 2.9. The transport by convection of water vapor from the warm, sintered grains below to the colder grains above. Condensation forms the prismatic laminar facets (Perla and Martinelli, 1979).

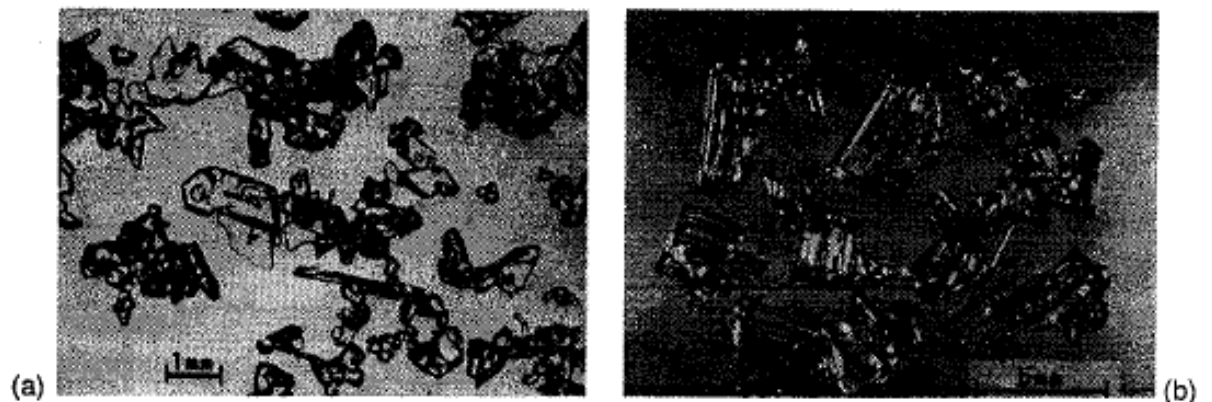


FIGURE 2.10. Temperature-gradient (TG) snow in successive stages of growth. Notice the change in scale from (a) to (b). (Reprinted with permission from Colbeck *et al.*, 1990. Photographs courtesy of K. Izumi.)

Suusa mudel

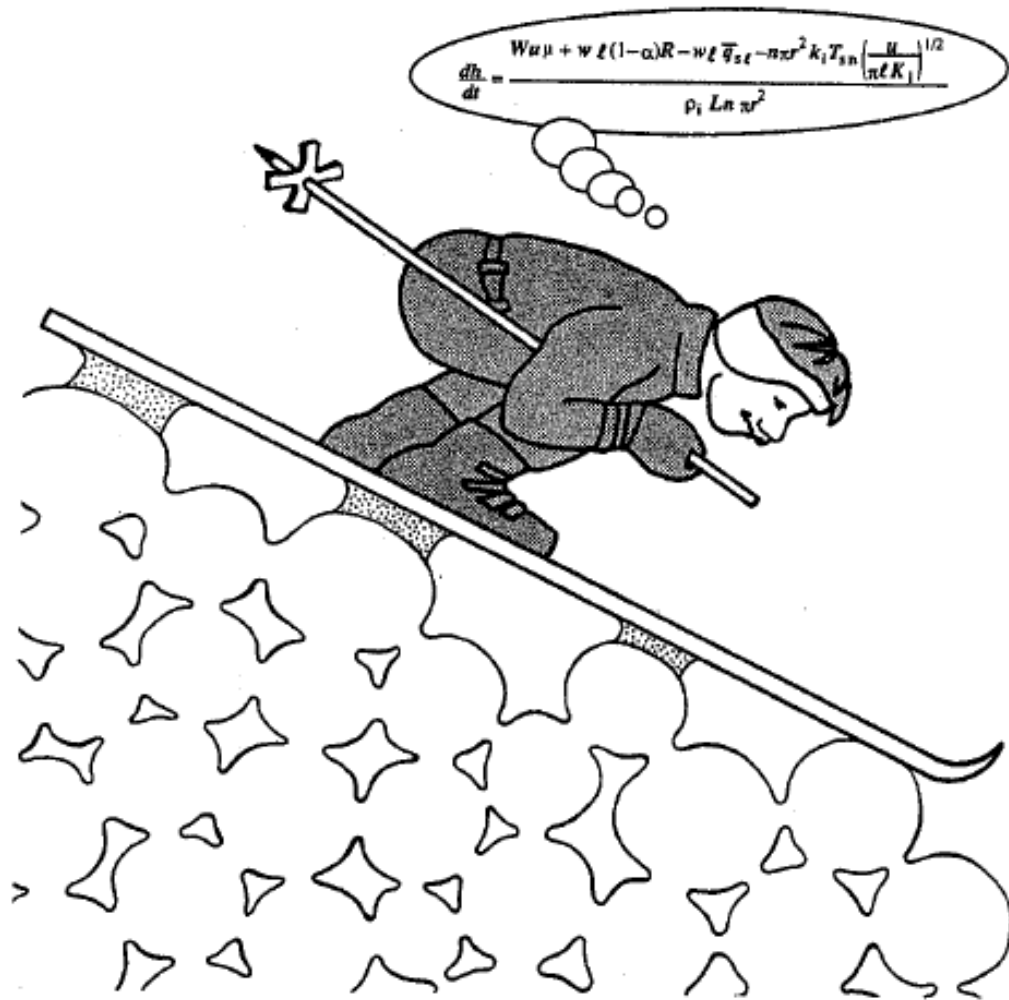


FIGURE 2.1. This skier heads down the hill, his skis lubricated by a film of water that forms under his skis. In his thoughts he mulls over a mathematical formula that we will discuss later in Chap. 8 on snow friction processes. (Colbeck, 1992. Drawn by Marilyn Aber, CRREL.)

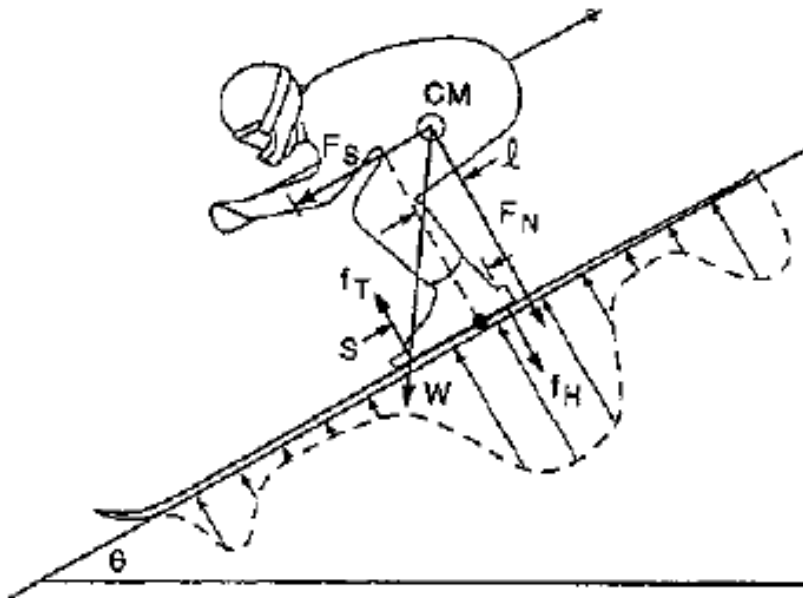


FIGURE 3.2. Forces acting on the ski through the boot.

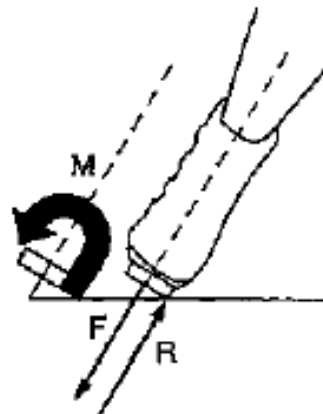


FIGURE 3.3. The lateral moment generated when the ski is set on edge.

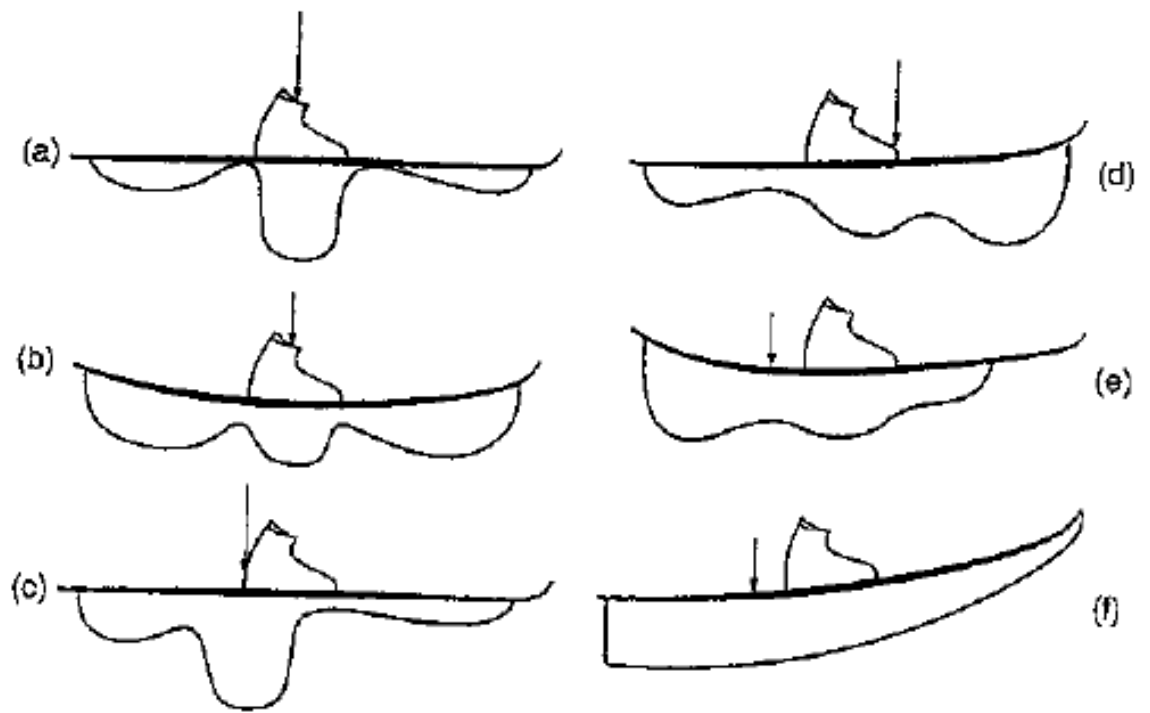


FIGURE 3.8. Bottom load distributions for six skis with different stiffness properties on snow beds of varied deformation.

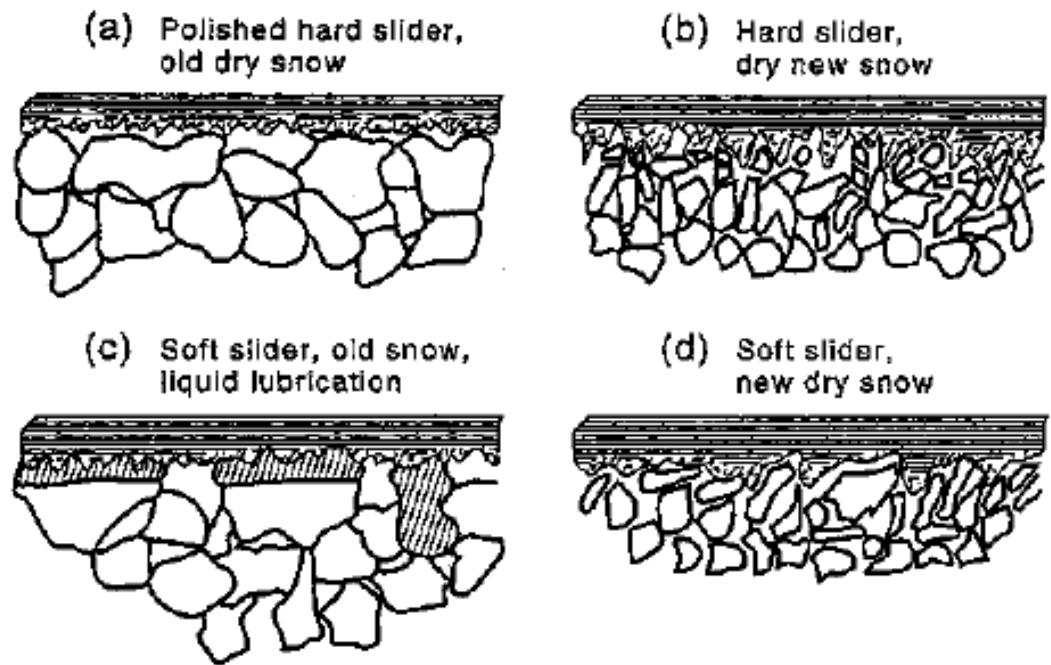


FIGURE 8.3. Four examples of the interactions that may occur at the interface of the ski bottom and the surface of the snow.

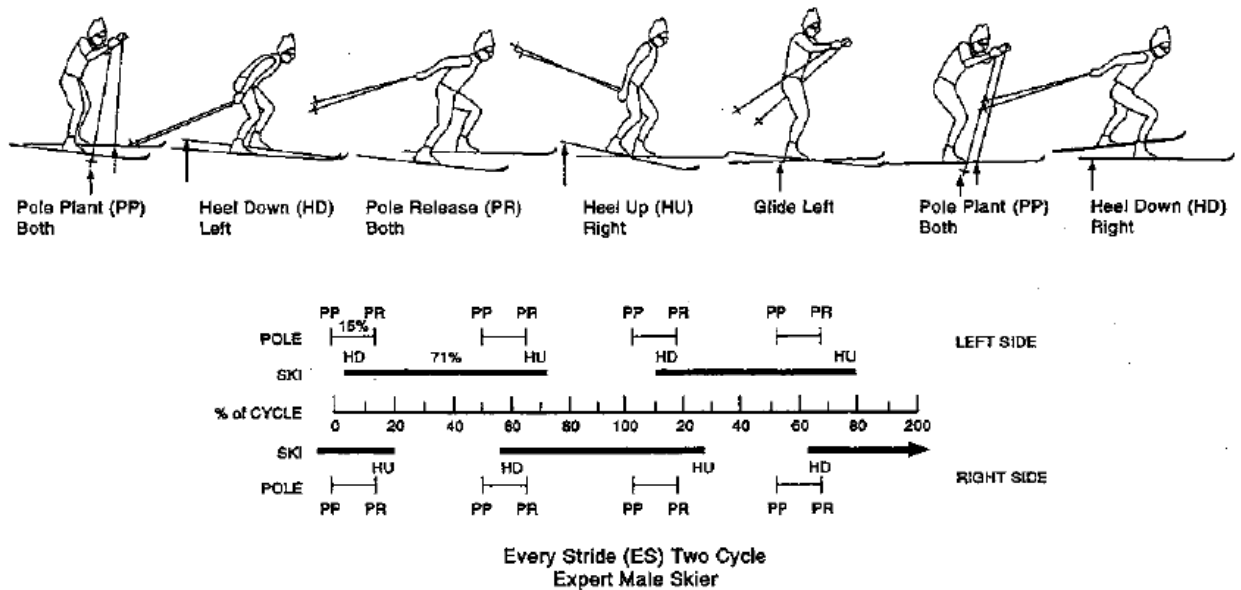
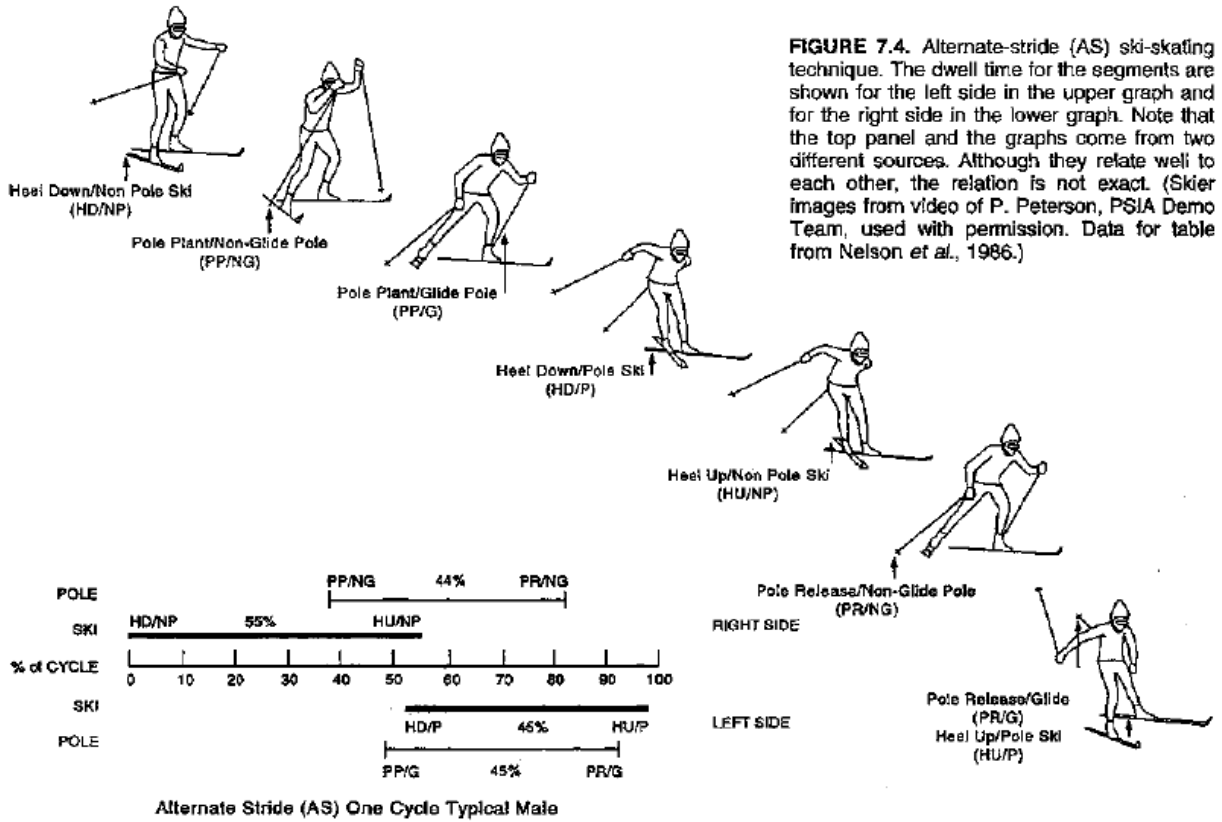
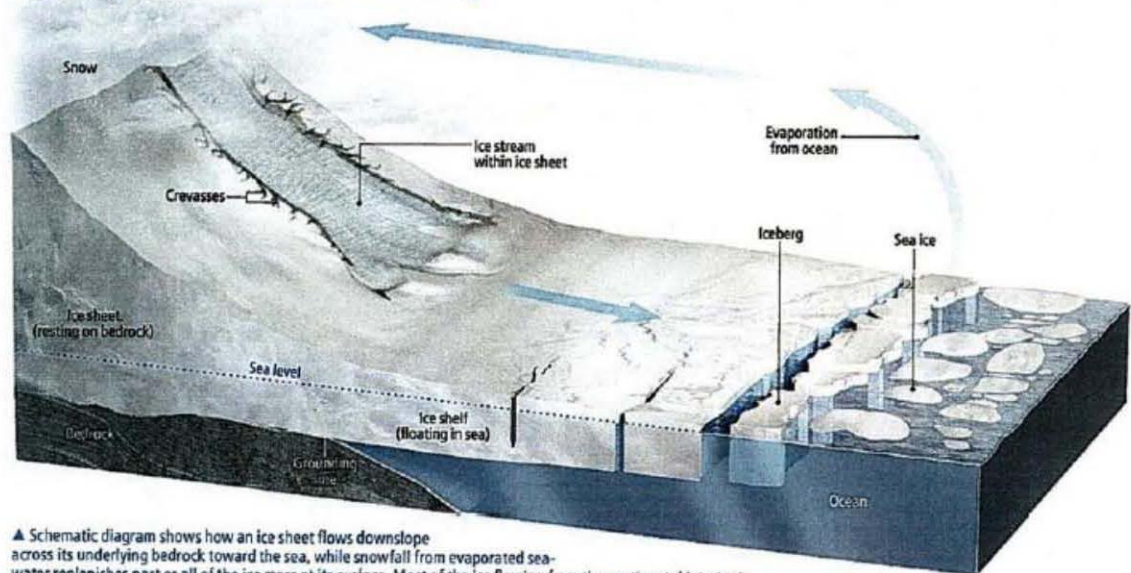


FIGURE 7.3. Every-stride (ES) ski-skating technique. The top panel shows the maneuvers for one half cycle. The lower graph shows the dwell time for each segment. Note that the top panel and the graphs come from two different sources. Although they relate well to each other, the relation is not exact. (Skier images from video of P. Peterson, PSIA Demo Team, used with permission. Data for the graph from Nelson *et al.*, 1986.)



[ICE MOVEMENT 101]

Steady State in a Frozen Country



▲ Schematic diagram shows how an ice sheet flows downslope across its underlying bedrock toward the sea, while snowfall from evaporated seawater replenishes part or all of the ice mass at its surface. Most of the ice flowing from the continental interior is carried to the sea by ice streams, relatively fast-moving conveyor belts of ice that break away from the surrounding sheet; the ice sheet travels seaward as well, albeit much more slowly. Once the base of the moving ice leaves its "grounding line," the floating ice is called an ice shelf, and it displaces a mass of water equal to its weight, raising the sea level accordingly. Throughout most of the past several millennia those processes did not raise sea level or shrink ice sheets because seawater evaporation and inland snowfall roughly balanced the discharge of ice into the sea.

Elastusteooria 3D

$$(\lambda + 2\mu)u_{1,11} + (\lambda + \mu)(u_{2,21} + u_{3,31}) + \mu(u_{1,22} + u_{1,33}) - \rho_0 \frac{\partial^2 u_1}{\partial t^2} = 0$$

$$(\lambda + 2\mu)u_{2,22} + (\lambda + \mu)(u_{3,12} + u_{3,32}) + \mu(u_{2,11} + u_{2,33}) - \rho_0 \frac{\partial^2 u_2}{\partial t^2} = 0$$

$$(\lambda + 2\mu)u_{3,33} + (\lambda + \mu)(u_{1,13} + u_{2,23}) + \mu(u_{3,11} + u_{3,22}) - \rho_0 \frac{\partial^2 u_3}{\partial t^2} = 0$$

u_1 u_2 u_3 – siirde komponendid

x_1 x_2 x_3 – koordinaadid

Navier- Stokes'i võrrandid hüdrodünaamikas, 3D

$$\rho \left[\frac{\partial u}{\partial t} + u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} + w \frac{\partial u}{\partial z} \right] = - \frac{\partial p}{\partial x} + \mu \left[\frac{\partial^2 u}{\partial x^2} + \frac{\partial^2 u}{\partial y^2} + \frac{\partial^2 u}{\partial z^2} \right] + F_x$$

$$\rho \left[\frac{\partial w}{\partial t} + u \frac{\partial w}{\partial x} + v \frac{\partial w}{\partial y} + w \frac{\partial w}{\partial z} \right] = - \frac{\partial p}{\partial x} + \mu \left[\frac{\partial^2 w}{\partial x^2} + \frac{\partial^2 w}{\partial y^2} + \frac{\partial^2 w}{\partial z^2} \right] + F_z$$

$$\rho \left[\frac{\partial v}{\partial t} + u \frac{\partial v}{\partial x} + v \frac{\partial v}{\partial y} + w \frac{\partial v}{\partial z} \right] = - \frac{\partial p}{\partial x} + \mu \left[\frac{\partial^2 v}{\partial x^2} + \frac{\partial^2 v}{\partial y^2} + \frac{\partial^2 v}{\partial z^2} \right] + F_y$$

u, v, w – kiiruse komponendid

x, y, z – koordinaadid

p – surve

μ – viskoosus

F_x, F_y, F_z – välisjõud

$$\rho \left[\frac{\partial \mathbf{U}}{\partial t} + \mathbf{U} \cdot \nabla \mathbf{U} \right] = -\nabla p + \mu \nabla^2 \mathbf{U} + \mathbf{F}$$

Magnetvoo jäävus

$$\oint_{\partial V} \mathbf{B} \cdot d\mathbf{a} = 0$$

Laengu jäävus

$$\frac{d}{dt} \int_V \rho_e \, dv + \frac{\delta}{\delta t} \int_{\sigma} w_e \, da = - \int_{\partial V} \mathfrak{J} \, da - \oint_{\partial \sigma} \mathbf{b} \cdot \mathbf{K} \, ds$$

Gaussi seadus (elektrivoog)

$$\oint_{\partial V} \mathbf{D} \cdot d\mathbf{a} = \int_V \rho_e \, dv + \int_{\sigma} w_e \, da + \oint_{\partial \sigma} \mathbf{b} \cdot \hat{\boldsymbol{\pi}} \, ds$$

Faraday seadus (elektromotoorne jõud)

$$\frac{1}{c} \frac{d}{dt} \int_S \mathbf{B} \cdot d\mathbf{a} + \oint_{\partial S} \mathbf{E} \cdot d\mathbf{x} = 0$$

Ampère'i seadus (magnetiline induktsioon)

$$- \frac{1}{c} \frac{d}{dt} \int_S \mathbf{D} \cdot d\mathbf{a} + \oint_{\partial S} \mathbf{H} \cdot d\mathbf{x} = \frac{1}{c} \int_S \mathfrak{J} \cdot d\mathbf{a} - \frac{1}{c} \int_{\gamma} \mathbf{b} \cdot \mathbf{K} \, ds$$

NB! A.C. Eringen, G.A. Maugin
Electrodynamics of Continua I, II
Springer, New York et al, 1990